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KINETIC ENERGY-MASS DISTRIBUTIONS FROM THE FISSION OF NUCLEI LIGHTER THAN RADIUM

F. Plasil, D. S. Burnett, H. C. Britt, and S. G. Thompson

July 16, 1965
KINETIC ENERGY-MASS DISTRIBUTIONS FROM THE FISSION OF NUCLEI LIGHTER THAN RADIUM

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ABSTRACT

The distributions in masses and total kinetic energies of fission fragments from a number of elements ranging from erbium to bismuth have been measured. The nuclei undergoing fission were produced by bombarding a variety of targets with projectiles ranging from He\textsuperscript{7} to O\textsuperscript{16}. The energies of coincident fission fragments were measured using solid state counters. The energy data were transformed to give mass-total kinetic energy density-of-events distributions. These distributions were compared with those calculated from an approximate version of the liquid drop model which applies to this region of elements. General agreement in the shapes and widths of the distributions was found particularly in the cases which involved small angular momenta and small nuclear temperatures. The dependence of the widths of the experimental distributions on the nuclear temperature was found to differ significantly from that predicted by the theory. Angular momentum effects were studied by using certain combinations of targets and projectiles to give the compound nucleus Os\textsuperscript{186} at the same excitation energy but with different angular momenta. The effect of increasing angular momentum was to broaden and change the shape of the experimental distributions.
I. INTRODUCTION

One consequence of the complex nature of the fission process is that there exists, at present, no generally accepted and adequate theory that is capable of accounting for all observed effects. In recent years, however, considerable progress has been made in the development of a theory of fission. Potential energy calculations made in the framework of the liquid drop model indicated that in the region of nuclei lighter than radium, an important approximation could be made. This approximation, which depends on the assumption that the shapes of the "liquid drop" nuclei at the saddle point can be considered as spheroids or a superposition of two spheroids, has made it possible for Nix and Swiatecki to work out the implications of this simple, well-defined model in a systematic way from initial conditions to final observable distributions using standard methods of statics, dynamics and statistical mechanics. In spite of the crude nature of a model that regards nuclei as drops of an incompressible uniformly charged liquid restricted to spheroidal shapes, the value of the approach becomes apparent when we remember that this is the first consistent attempt to reproduce the entire fission process through all its stages yielding from first principles calculated distributions, such as the mass-total kinetic energy distributions, that may be compared directly with measured distributions.

The purpose of this work is to provide data for nuclei of $A \lesssim 220$ where the Nix-Swiatecki theory is expected to apply, and to compare these results with the theoretical results. The restriction of the region of applicability to relatively light elements introduces an experimental problem; namely, that of small fission cross sections. There are, however, two effects which tend to increase fissionability and make such measurements feasible; namely, (a) high angular momenta such as are encountered in heavy ion reactions and (b) high excitation energies. The high angular momenta, while increasing the fissionability, introduced several complications. The most serious of these is that the Nix-Swiatecki theory, with which the results have been compared, has been developed only for the case of zero angular momentum. An attempt has been made to isolate the effects of angular momentum by comparing the results from the fission of the $^{186}$Os compound nucleus produced by $^{4}$He $+ W^{182}$ with that produced by $^{16}$O $+ Er^{170}$ at the same excitation energy.

The high excitation energies required to induce fission do not complicate comparison of experimental and theoretical results. The theory covers the
whole range of excitation energies encountered in this work and makes definite predictions concerning variations in the resulting fission distributions with nuclear temperature. In order to test these predictions, measurements have been made at several bombarding energies for each combination of target and projectile.

The projectiles used were $^{16}\text{O}$ (from 102 to 165 MeV bombarding energy) and $^4\text{He}$ (from 40 to 120 MeV). Two distributions from $^{12}\text{C}$ bombardments were also measured. The range of targets extended from Er$^{170}$ to Bi$^{209}$. In all cases the energies of pairs of fission fragments from the same fission event have been measured with semiconductor detectors and recorded in a correlated manner. The resulting energy versus energy distributions have been converted to mass versus total kinetic energy distributions. These, in turn, have been compared directly with similar distributions calculated from the Nix-Swiatecki theory.

II. EXPERIMENTAL

The experimental techniques and the method of data processing were in many ways similar to that of Haines and Thompson$^4$ and have been described in detail in earlier reports.$^5,6,7$ A beam of alpha particles or heavy ions defined by two or more circular collimators of 2 mm diameter and up to 18 inches apart struck a thin target at the center of a circular fission chamber. Two collimated semiconductor detectors were mounted on radial arms inside the chamber. One of the detectors subtended an angle of $3^\circ$-$4^\circ$ at the center of the chamber and was placed typically at $60^\circ$ with respect to the beam direction. This choice was made because the angle subtended allowed a reasonable counting rate and yet defined the detector position sufficiently well to make insignificant the dispersions resulting from angular uncertainty. While one angle had to be defined in this way to satisfy a condition imposed by center-of-mass transformations,$^5$ the other detector subtended an angle of $15^\circ$ to $20^\circ$ which was large enough to collect all fission fragments in coincidence with the first detector.$^6$ The angular position of this large detector was typically $90^\circ$ with respect to the beam direction, its exact position being determined for each bombardment by making a rough angular correlation measurement. Permanent magnets were placed in front of the two detectors to eliminate interference from low energy electrons. Heavy ion beams of $10.3 \pm 0.1$ MeV per nucleon were obtained from the Berkeley Heavy Ion Linear Accelerator (Hilac).
Aluminum foils were used to degrade the beam to the energy needed. Range-energy curves of Northcliffe were used for this purpose. Helium ion beams were obtained from the Berkeley Variable Frequency 38" Cyclotron. In this case energy degradation was not necessary since the accelerator produced particles of the required energies directly. The beam currents used were less than 20 millimicroamperes (mµa) in the heavy-ion bombardments and up to 100 mµa in the cyclotron bombardments. The difference is due to the low duty cycle of the Hilac and the larger energy deposition of the scattered heavy ions in the depletion layer of the detector, which combined to decrease the energy resolution substantially at beam levels above 20 mµa.

The following targets were used in this study: Er\textsuperscript{170}, Yb\textsuperscript{174}, W\textsuperscript{182}, Au\textsuperscript{197} and Bi\textsuperscript{209}. The erbium, ytterbium and tungsten enriched (90-99%) isotopes were obtained in oxide form from the Oak Ridge National Laboratory, converted to fluoride by precipitation from nitric acid solution and evaporated from a molybdenum crucible by means of electron bombardment onto thin Ni foils. The commercial Ni foils had nominal thicknesses of 90 to 135 µg cm\textsuperscript{-2}. The gold and bismuth targets were also prepared by evaporation, but were self-supporting, with the exception of those used in experiments 1 and 6 of Table I, ranging in weight from 100 to 200 µgms cm\textsuperscript{-2}. The data were corrected for the finite target thickness by using the relationship $\Delta E_t = cE^{1/3}$, where $E$ is the fragment energy, $c$ is a constant and $\Delta E_t$ the loss of energy due to target thickness. This relationship is based on the work of Alexander and Gazdik. The constant $c$ was determined for any particular target by measuring fission distributions at several values of the angle between the detector and the target plane. Errors from this source in the final energy spectra may have been as high as 0.8 MeV for the most unfavorable cases.

Several types of detectors have been used in this work, all with similar response characteristics and resolution. Gold surface-barrier silicon detectors with 150 Ω-cm resistivity were used in the heavy-ion-induced experiments. They were operated at a reverse bias of 10-15 V. At this bias all fission fragments are stopped in the depletion layer of the detector, but the scattered heavy ions, which cause an undesirable background of pulses, do not deposit all of their energy. In the cyclotron experiments phosphorus-diffused semiconductor detectors of 200-400 Ω-cm resistivity were typically used. They were operated at a bias of 100-150 V. In this mode of operation both types of detectors showed good energy resolution as measured with fission fragments from
the spontaneous fission of $^{252}\text{Cf}$ before and after each experiment. The detectors were supplied by W. Hansen of this laboratory. The leakage current in the detectors was continuously monitored during each run. It was found to increase rapidly when radiation damage became appreciable. This was sometimes found to be the case during bombardments with heavy ions over a long period of time. Detectors with currents greater than 3 $\mu$A were always replaced. The calibration of the detectors will be discussed in the next section.

The electronic equipment consisted of two linear amplification systems, a fast and slow coincidence system and a multiparameter pulse-height analyzer with a magnetic tape recording unit. The analyzer used during the heavy-ion experiments was a locally built machine, and that used during the cyclotron experiments (with one exception mentioned in Section IV) was a Nuclear Data analyzer, model ND 160, with a buffer memory and tape unit. The linear amplification system was maintained at a high level of stability. This stability was continuously monitored during each run by means of a high precision mercury pulse generator which fed pulses through the entire system. The maximum drift during any run was under $1/\mu$, and no corrections to the data were found to be necessary. The outputs of the two linear systems went directly to the multiparameter analyzer. The fast coincidence system was of such time resolution (about 20-30 nsec) as was required to eliminate accidental events, but gave an output pulse every time both fragments from a single event were detected. This output was delayed and fed into a slow coincidence unit, which also required the presence of the two linear pulses. The output of this unit activated the multiparameter analyzer in the case of the heavy-ion experiments, and it opened gates allowing the linear pulses to reach the analyzer in the cyclotron experiments. In the experiments at the Hilac, Model VI Goldsworthy\textsuperscript{11} linear amplifiers and pre-amplifiers were used, together with several Hewlett-Packard distributed amplifiers and transistorized coincidence units. In the cyclotron experiments pulse shaping, amplification, fast and slow coincidence and linear gating were all performed in one unit designed by F. S. Goulding and D. Landis.\textsuperscript{12} Two dimensions of the multiparameter analyzer were used, one for each of the two fission fragments. The data were stored event by event on magnetic tape in such a way that pairs of pulse heights, corresponding to any one given fission event, were kept together. Thus the number of events $N(P_1, P_2)$ in which fragment 1 produced a pulse height $P_1$ and fragment 2 produced a pulse height $P_2$ was measured for all combinations of $P_1$.
and }_2^0\text{, resulting in a two-dimensional number-of-events distribution. The magnetic tapes were processed on IBM 7090 and 7094 computers.}

The total number of events measured in any one distribution ranged from \(2 \times 10^4\) to \(2 \times 10^5\). In the case of heavy-ion reactions very slow counting rates were encountered making it sometimes necessary to add together data from several experiments. In the case of the cyclotron experiments several distributions were remeasured at different times to check reproducibility and consistency. The reactions studied and the numbers of events recorded are given in Table I.

III. CALCULATIONS

A. Calibration of Semiconductor Detectors

Several methods of calibration of semiconductor detectors have been considered during the course of this work.\textsuperscript{6,7} The most successful method in the early stages of this study was one that takes advantage of the large center-of-mass effect in heavy-ion bombardments. Due to this effect fission fragments at forward angles have a considerably higher kinetic energy than those at backward angles.\textsuperscript{4,5} The fission spectrum resulting from the reaction \(\text{Bi}^{209} + (165\text{ MeV}) \text{O}^{16} = \text{Pa}^{225}\) was measured at several angles. The average positions of these spectra defined the energy calibration for fragments of mass 112. The energy calibrations for other masses depended on the construction of lines parallel to the mass 112 line in an energy pulse-height diagram. The spacing of the lines was determined on the basis of the two peaks from spontaneous fission of \(\text{Cf}^{252}\).\textsuperscript{13,14}

In the later stages of this work, a comprehensive and consistent method of calibrating semiconductor devices became available from the extensive work of Schmitt, Kiker and Williams.\textsuperscript{15} Their method makes the intercept as well as the slope of calibration equations dependent on mass according to the equation:

\[
E = (a + a'M)x + b + b'M,
\]

where \(E\) is the energy of the detected particle, \(M\) its mass and \(a\), \(a'\), \(b\) and \(b'\) are constants. The values of these constants are the same for all detectors of the type used by these authors, and the values quoted by them were used in this work. The method of calibration used in all the cyclotron work was identical to that suggested in Appendix II of reference 15. In the heavy-ion
work the first method of calibration was used as described above, but a
careful comparative study of the two methods showed them, for practical
purposes, to give identical results (within 1.0% for all quantities of
interest).

B. Transformations

While the primary data may be viewed as a density distribution of
events in a pulse-height 1 versus pulse-height 2 plane, the above calibration
together with a correction for the loss of energy of the fragments due to
the finite thickness of the target transforms this distribution into one that
has the two measured fragment energies as the new coordinates. By means of
a center-of-mass correction and a random number technique, the coordinates
may be changed to $E_1^*$ and $E_2^*$ where the energies are now center-of-mass
energies, and the asterisk identifies quantities measured after the emission
of neutrons. A further transformation made use of conservation of momentum
in fission from which the expression $A_1/A_c = E_2/E_T$ may be derived. Here $A_1$
and $A_c$ are the masses of fragment 1 and the compound nucleus respectively, and
$E_2$ and $E_T$ are the energy of fragment 2 and the total kinetic energy of both
fragments respectively.

We replaced the above exact expression with the approximate relation:

$$A_1 \simeq \frac{(E_2/A_c)}{(E_1^* + E_2^*)}.$$

The error introduced by replacing pre-neutron emission energies with post-
neutron emission energies is very small and is discussed fully in reference 7.
The new coordinates of the measured distributions $P(E_T^*, A_1)$ are, thus, the
mass (before neutron emission) of fragment 1, $A_1$, and the total kinetic energy
(after neutron emission) released in the process ($E_T^*$).

C. Statistical Calculations

The measured distributions $P(E_T^*, A_1)$ have been analyzed in terms of
their first and second moments. These have been calculated for the overall
distributions in one variable (e.g. mass-yield curves) as well as for the
distributions in one independent variable taken as a function of the other
variable (e.g. mass-yield curves for a set of $E_T$ values). The first moment,
\( \mu_1(x) \) of a distribution in a variable \( x \) is the mean of the distribution \( \langle x \rangle \). The second central moment is the variance \( \mu_2(x) \) which is the measure of the width of the distribution \(^{16}\) and is given by:

\[
\mu_2(x) = \langle x^2 \rangle - \langle x \rangle^2.
\]

The fourth moment \( \mu_4(x) \) was also calculated and used in estimating statistical standard errors in the second moments.

The distributions were not "folded", i.e., the symmetry of mass distributions has not been forced. This gave a valuable check on the data. Reference 6 discusses the symmetry properties that the distributions had to satisfy.

D. Neutron Emission Effects

The emission of neutrons has to be considered in two ways:

(a) Pre-fission neutron emission from the compound nucleus introduces an uncertainty in the excitation energy, and hence the nuclear temperature at the time of fission. A knowledge of the nuclear temperature is required for a comparison of experiment with theory, and this effect will be considered in Subsection E.

(b) The effect that neutron emission from the fragments has on the shape of the mass-total kinetic energy distributions \( P(A_1, E_T) \), in general, and on the values of moments of these distributions, in particular, is of great importance since the theoretical distributions do not take neutron emission into account. Although for any given combination of values of \( A_1 \) and \( E_T \) there is a distribution in the numbers of neutrons \( v_1 \) and \( v_2 \) emitted from the two fragments, we have neglected this as well as any correlation of \( v_1 \) and \( v_2 \) with \( A_1 \) and \( E_T \), i.e., we assume \( v_1 = v_2 = v_T/2 \). The formulae used to correct the moments and to calculate \( v_T \), together with an outline of their derivation, are given in Appendix I. They are based on the method of Haines.\(^5\) The most important correction is that made to the absolute magnitude of the total kinetic energy, \( E_T \). The extent of this correction can be seen from the data tabulated in Table I. Neutron emission from the fragments also enters into the calculation of \( A_1 \) discussed earlier. Errors from this source are small since the approximation \( E_1/E_T \approx E_1^*/E_T^* \) is a good one. It gives exact results for the case \( v_1 = v_2 \) and introduces a maximum error of only one or two mass units if \( v_1 \) and \( v_2 \) are very different.
The effect of neutrons on the widths of the overall distributions (mass-yield and \(E_T\)-yield curves) is appreciable. Corrected and uncorrected results will be given. The effects of neutrons on variances of conditional distributions such as \(\mu_2(A_1)\) and the variance of the mass distribution as a function of \(E_T\) are remarkably small. Uncorrected results will be presented. In the case of \(\langle E_T \rangle\) considered as a function of mass, the only effect is in the absolute value of \(E_T\), and corrected results will be given.

An alternative approach to the question of prompt neutron emission from fission fragments has also been explored. This method attempts to transform entire distributions rather than just the statistical moments. The main problem of such a transformation is that the manner in which the deformation energy at the saddle divides between the two fragments for every event considered must be known. This information, while at present unavailable experimentally, is a product of the Nix-Swiatecki theory. It is therefore possible to invert the problem and "fold in" neutron effects into the theoretical calculations. The theoretical calculations are thus made to take the exact form of the measured distributions (excluding only angular momentum effects). These calculations have been performed, for several cases, using a Monte Carlo technique. The method and results are given in Appendix II. The results compare favorably with those from the more conventional approach of Appendix I, and the discussion and conclusions in this work are unaffected by the choice of method of correction.

E. Theoretical

Mass-total kinetic energy probability distributions, which can be compared with the measured \(P(A_1, E_{T*})\) density-of-events distributions, have been calculated directly from the theory of Nix and Swiatecki. In this theory, which in its present state of development holds only for the case of zero (or low) angular momentum, the compound nucleus is considered to be an irrotational, uniformly-charged liquid drop. Its shape is restricted to that of a spheroid or to two spheroids, which may be overlapping or tangent to each other. The potential energy surface was calculated by Nix and Swiatecki in this parametrization. Classical equations of motion were solved, allowing the liquid drop in an initial state of motion to be followed, in terms of its energy and deformation, through the scission and fragment separation processes to infinity. The assumption of statistical equilibrium at the saddle gave a
distribution of initial conditions which was combined with the relationship between these conditions and final observable quantities to produce expressions for the mass-total kinetic energy probability distribution. The remarkable feature of this theory is that a simple model has been consistently followed through the entire fission process and that there are no adjustable parameters involved when comparisons with experiments are made. An important step in the development of the theory is the expansion of the potential energy about the saddle point. This expansion is required for the calculation of the probability distributions for initial conditions. When only harmonic terms are retained, quantum mechanically correct results may be obtained. These results are the most accurate available at very low nuclear temperatures. In this work, however, temperatures were relatively high so that classical statistical mechanics is valid for determining the initial conditions. Under these circumstances Nix and Swiatecki have found it possible to retain anharmonic terms in the potential energy expansion, and these were found to have a significant effect on the final calculated distributions. The theoretical distributions used in this work include anharmonicity effects, in contrast to those used in references 6 and 7. All theoretical curves shown in the figures were obtained by numerical means from the appropriate expression for $P(A, E_T)$ given in reference 3.

The widths of theoretical distributions are dependent on the nuclear temperature at the saddle point. As was indicated, pre-fission neutron emission complicates the calculation of the excitation energy, and hence also the calculations of the nuclear temperature. This problem was thought to be most serious in the case of heavy-ion bombardments. Calculations based on the analysis of measured excitation functions, however, indicated that the average number of pre-fission neutrons was relatively small $(0.2 - 1.5)$. These calculations involved the evaluation of branching ratios between fission and neutron emission along the neutron evaporation chains, using modified level widths expressions of Huizenga and Vandenbosch. These branching ratios, which were evaluated at many fixed values of angular momentum, involve the fission barrier and level density parameters. The fission barrier and the level density parameters were both left adjustable, although the functional variation of the fission barrier with angular momentum was taken from the calculations of Cohen, Plasil and Swiatecki. Partial probabilities for fission at given
values of angular momentum and at various stages of the neutron evaporation chain were evaluated by means of the branching ratios. These partial probabilities were integrated numerically over a classical angular momentum distribution and over the neutron evaporation chains, giving a total fission cross section. This calculated cross section was then fitted, together with other calculated cross sections at different excitation energies, to excitation functions of Sikkeland by adjusting the variable parameters mentioned above. The calculations computed such quantities as the average number of pre-fission neutrons and the average excitation energy at the saddle. These results were used to calculate nuclear temperatures for the various heavy ion cases. A similar study was carried out for the case of He$^4$ + Au$^{197}$. The pre-fission neutron-emission effects were even smaller, and they were consequently neglected. Details of the heavy-ion calculations may be found in reference 7.

The equation of state,

$$E_x^S = a \theta^2 - \theta,$$

which relates the nuclear temperature at the saddle, $\theta$, to the excitation energy at the saddle, $E_x^S$, was used. In this expression, $a$ is the level density parameter, taken to be equal to $A_c/\bar{B}$. $E_x^S$ is given by

$$E_x^S = E_x - B_f,$$

where $E_x$ is the excitation energy of the compound nucleus as calculated from Cameron's masses, and $B_f$ is the liquid-drop fission barrier corrected for ground-state shell effects. In the heavy-ion induced fission, where use of the above neutron evaporation calculations has been made, $E_x^S$ was a quantity averaged over the angular momenta and the numbers of pre-fission neutrons involved. A tabulation of $\theta$ values is given in Table I.
IV. PRESENTATION OF EXPERIMENTAL RESULTS

The reactions studied, the total number of events measured, the nuclear temperatures at the saddle point, and the first and second moments of the overall distributions, both corrected and uncorrected for neutrons, are tabulated in Table I. The order in which experiments were performed is also given. As can be seen, several experiments have been repeated at different times in an effort to establish reproducibility for small changes in experimental conditions (e.g., different detectors and amplifier gains). The error estimates given in the table have been obtained primarily from these duplicate measurements and from the scatter in the data when examined as a function of excitation energy. As was noted in Section II, some heavy-ion reactions involved such low counting rates that it was in some cases necessary to add together data from several runs. Variations between individual runs making up the total distributions were used to estimate the errors given in Table I for the heavy-ion-induced-fission cases. In all cases errors due to counting statistics were very much smaller than systematic errors. An important point is that the data from fission of Bi$^{209}$ induced with 65 MeV He$^4$ ions were obtained considerably earlier than the rest of the He$^4$ data. Several changes in technique make this point an entirely independent experiment. (Instead of the equipment described in Section II, this experiment involved the use of a nickel-backed bismuth target, detectors of 1700 Ω-cm resistivity, Goldsworthy Model VI amplifiers, a slow coincidence instead of a fast-slow coincidence system and a different multiparameter analyzer. Furthermore, the method of calibration was not that of Schmitt, et al., but was based on the alpha particles as well as on the fission fragments from a Cf$^{252}$ source.) The 65 MeV data agree within the quoted limits with those obtained by interpolation from the later experiments. This is further evidence for the likelihood that the quoted errors are realistic estimates of the actual systematic errors and gives us some confidence in comparing the Hilac and cyclotron data taken under considerably different experimental conditions as discussed in Section II.

Six types of figures have been used to present the data. These consist of:

(i) mass-total kinetic energy contour diagrams (Figs. 1-3),
(ii) overall distributions such as mass-yield and total kinetic energy-yield distributions (Figs. 4-7),
(iii) variances of the overall distributions as a function of nuclear temperature (Figs. 8-11),
(iv) the average total kinetic energy, \( \langle E_T \rangle \), as a function of mass (Figs. 12-13),
(v) the variances of the total kinetic energy distributions, \( \mu_2(E_T) \), as a function of mass (Figs. 14-15) and
(vi) the variances of the mass distributions, \( \mu_2(A_1) \), as a function of the total kinetic energy (Figs. 16-17).

With the exception of Figs. 8, 9, 12 and 13, the experimental results have not been corrected for neutron effects. In the case of Figs. 12 and 13, an uncorrected curve is essentially identical to that shown, except for an overall decrease in magnitude of the entire experimental curve. The corrected curves of variances of conditional distributions (Figs. 14-17) are only slightly lower in magnitude than those presented in the figures.

The most complete method of presenting a mass-total kinetic energy distribution is in the form of a contour diagram. Such diagrams are shown in Figs. 1-3. The contour lines pass through regions of constant density-of-events in the experimental case, and through regions of constant probability of finding an event in the theoretical case. The advantage of this presentation is that all available information is included on a single diagram.

For any given combination of projectile and target, the average overall total kinetic energy is constant, within experimental limits, for all excitation energies studied. For this reason, it was possible to normalize the overall yield-total kinetic energy distributions shown in Figs. 4-7 in such a way as to make, for any given type of reaction, the overall \( \langle E_T \rangle \) at all values of the nuclear temperature equal to \( \langle E_T \rangle \) at the lowest temperature. Such normalization in Figs. 4-7 was necessary to adequately illustrate the effect of temperature on the widths of distributions.

As was discussed earlier, the theoretical expressions which apply to the relatively high nuclear temperatures encountered in this work are not expected to hold at very low temperatures. For this reason, the theoretical curves of Figs. 8 and 10 extend only over the range of temperature which applies to the experiments presented in this work.
V. DISCUSSION

In Section II the measurement of two-dimensional density-of-events distributions, which had as co-ordinates the pulse heights produced by both fission fragments from any given event, have been described. Section III outlined the method by which these distributions have been transformed to mass-total kinetic energy distributions $P(A_1, E_{T*})$. The basic features of the Nix-Swiatecki theory which yields similar distributions from first principles have also been described. In Section IV the experimental results have been presented, and in the remainder of this section the theoretical and experimental distributions will be compared.

A number of important points must be borne in mind during the course of the discussion of results and comparisons with theory. The first of these is the fact that the theory does not include the use of any adjustable parameters. The experimental distributions have not been normalized to the theoretical ones in any way. The size, surface tension and charge of the idealized liquid drops of Nix and Swiatecki are those which apply to actual nuclei as determined from Green's analysis of ground-state masses. Comparisons with experimental results from the fission of real nuclei do not involve the introduction of new parameters since all other quantities are calculated directly from the model.

The second point concerns the question of angular momentum effects. During the course of a bombardment that involves any particular combination of target, projectile and bombarding energy, the projectile may strike the target with varying impact parameters. Thus, the angular momentum ranges from zero to some maximum value, which may be as large as 100 units of $\hbar$ in the cases of heavy-ion bombardments. Due to the existence of such angular momentum distributions and the fact that the theory at this stage has not concerned itself with this problem at all, we shall content ourselves with a qualitative discussion of this effect. When we consider the various distributions in the case of the calculations of saddle-point excitation energies mentioned in the last section, however, the angular momentum effects have been dealt with quantitatively.\footnote{7}

The last point to be recalled is the fact that the measured $P(A_1, E_{T*})$ distributions are obtained after the emission of neutrons from the fragments, whereas the theory refers to pre-neutron emission energies. While it is
difficult to correct the entire experimental distribution in such a way as to obtain a pre-neutron emission distribution, the correction of the statistical moments, and of the entire theoretical distributions, is somewhat easier. In the first method, however, approximations have to be made in the derivations of the necessary formulae,\(^6\) while the second method, although consistent within the framework of the theory, nevertheless, requires the theory to describe adequately not only the mass and total kinetic energy distributions of interest in this work, but also the distributions of excitation energies of the fragments. Thus, both methods must be viewed with some caution. For these reasons, when whole distributions are shown, they are not corrected for neutron effects, while when moments of overall distributions are presented, both corrected and uncorrected results are given. The moments of conditional distributions are, in general, uncorrected, but the corrected results are not very different from uncorrected results.

The comparisons have been made as a function of the magnitude of two important variables: (a) the temperature of the compound nucleus in its saddle configuration and (b) the angular momentum of the compound nucleus. As was discussed above, the first of these two effects is an essential feature of the theoretical calculations, while the second effect has not been considered by Nix and Swiatecki in the present state of development of their theory.

General agreement between experiment and theory can be found in several features of the distributions, although some areas of agreement are restricted to only a portion of the experimental data. The theoretical prediction of the overall average total kinetic energy, \(\langle E_T \rangle\), is very good, and agreement is found for both heavy ion and \(\text{He}^4\) results, as can be seen from Table I. Examination of the contour diagrams reveals that the theory correctly predicts a general triangular appearance of the distributions, although the heavy-ion distributions tend to be elliptical rather than triangular. The shape of theoretical and experimental overall mass-yield and total kinetic energy-yield curves is similar, and their widths agree, within experimental errors, in about half of the cases studied. Concerning the moments of the conditional distributions presented in Figs. 12 to 17, agreement may be found in the \(\text{He}^4\)-induced-fission cases, particularly at low bombarding energies.
A. Temperature Dependences

The fact that the Mix-Swiatecki theory has not been developed to the point of including angular momentum effects makes it more appropriate to compare the theory with the $\text{He}_4^4$ data than with the heavy-ion induced data. For this reason the discussion will initially be restricted to the $\text{He}_4^4$ data, while the heavy-ion data will be considered separately later.

An examination of the contour diagrams for the fission of $\text{At}^{213}$ produced by a $\text{He}_4^4$ bombardment of $\text{Bi}^{209}$ (Fig. 1) shows that as the temperature increases, both experimental and theoretical distributions broaden, and the triangular shapes of the measured distributions tend to show more rounded corners. It is interesting to note that while the width of the measured distributions increases more slowly than that of the calculated distributions, the discrepancy is greater in the $E_T$ direction than in the mass direction. This point is illustrated in Figs. 4 and 5, where the overall distributions are presented. Thus, for example, in the extreme case there is little difference between the $E_T$-yield curves from the reaction $\text{Au}^{197} + \text{He}_4^4 = \text{Tl}^{201}$ measured at laboratory energies of 60 or 120 MeV. The differences in width between the mass-yield curves is greater, but not as great as that predicted by theory. Figures 8 to 11, which show the widths of the overall distributions as a function of temperature provide a summary of the temperature broadening effect. In the $\text{He}_4^4$ induced cases, the results which are uncorrected for neutron effects (Figs. 10 and 11) provide better agreement between experiment and theory than those which are corrected for neutron effects (Figs. 8 and 9). While the method used in these corrections does include approximations, the direction of the effect, i.e., a broadening of measured distributions due to prompt neutron emission, is nevertheless correct, and the results therefore tend to point to a real disagreement between experiment and theory. The widths of mass distributions in these $\text{He}_4^4$ bombardments broaden as predicted up to about 80 MeV bombarding energy. Beyond this energy the width does not increase with temperature as rapidly as predicted. For the same reactions the widths of the overall $E_T$ distributions as a function of temperature present an even greater problem. They are too large at low temperatures and too low at high temperatures. In the $\text{Au}^{197} + \text{He}_4^4$ case, for example, the plot of the experimental variance of $E_T$ versus $\theta$ is, in fact, virtually flat.

The "washing out" of the triangular distribution shape has been pointed out in Fig. 1. This effect is also present in Figs. 14 and 16, which give the
widths of conditional distributions for the Bi$^{209} + \text{He}^4$ case. The tendency of the $\langle E_T \rangle$ versus mass curves of Fig. 12 to flatten with increasing nuclear temperature should also be noted. If these effects were merely due to poor experimental resolution, it would be expected that they would be more prominent in the distributions measured at lower bombarding energies, due to the most difficult experimental conditions which result from lower cross sections. The experimental results show just the reverse trend to hold.

It must be remembered that as bombarding energy increases, not only the temperature but also the average angular momentum increases. As will be discussed later, some of the effects due to angular momentum tend to be similar to those due to high temperatures. It is therefore difficult to separate one cause from the other as far as the "washing out" of the triangular distributions is concerned. The general conclusion of the above discussion, namely that the widths of the measured distributions do not appear to increase as fast with nuclear temperature as predicted by the theory, is, however, independent of any angular momentum considerations since larger angular momenta tend to broaden distributions.

Before the lack of agreement in temperature dependent features is assigned to shortcomings of the theory, several possible contributing causes should be examined. These all depend in one way or another on uncertainties in the nuclear temperature. The first problem could be that the equation of state that we have chosen to relate $\Theta$ to the excitation energy might not apply in some regions of this study. The evidence that shows that this is not likely to be the only explanation is the fact that almost no change in the widths of experimental $E_T$-yield curves is observed in the He$^4$ bombardments ranging from bombarding energies of 80 MeV to energies of 120 MeV. This would imply that the expression for $\Theta$ is independent of excitation energy in this region. The next possibility is a large contribution at high He$^4$ energies from fission following direct interactions. Excited nuclei created in this manner do not all possess all of the energy and momentum of the projectile, causing the temperature to be lower than calculated. The distribution widths at high energies would, therefore, be lower than expected, as is indeed the case. The possibility that this effect is a contributing factor was eliminated by a careful angular correlation study in the appropriate energy region. No evidence of fission following incomplete momentum transfer was found. A
further possibility is that at high energies a considerable number of neutrons is evaporated from the compound nucleus prior to fission, thus reducing its temperature. The measurement and analysis of the fission excitation function of Tl$^{201}$ provided us with level density parameters and the fission barrier for this case. Using these values we extended the calculations of reference 23 to high energies and included effects of de-excitation through a neutron evaporation chain. It was found that the number of neutrons emitted prior to fission was not large. The calculated fission cross sections, compared with measured cross sections, however, no longer agreed at these high temperatures, regardless of whether neutron evaporation effects were included or not. This made the analysis inconclusive, and the possibility of a large amount of neutron evaporation prior to fission cannot be ruled out. A study of angular distributions at high energies, which could yield independent determinations of $\theta$ at the time of fission would be of interest.

The following conclusion becomes apparent: while the accuracy of the determination of nuclear temperature is lowered due to a number of sources of possible error, the uncertainties in the temperature do not appear to be large enough to alone account for the difference between experiment and theory. Thus the theory seems to predict too rapid a temperature dependence.

From an examination of Fig. 6, where the $^{182}W + ^{16}O$ reaction is presented, and from the heavy ion data in Figs. 8-11, there appears to be little disagreement between experiment and theory as far as temperature dependency is concerned. This agreement, however, is probably fortuitous in that it may be caused by the broadening effects of angular momentum, which are described in the next subsection.
B. Angular Momentum Effects

The two reactions $^{182}$W + $^4$He = $^{186}$Os and $^{170}$Er + $^{16}$O = $^{186}$Os are particularly useful in determining the effect of angular momentum on the measured distribution. Using $^{16}$O ions of 165 MeV energy and $^4$He ions of 120 MeV, the nuclear temperature at the saddle is approximately equal (2 MeV), and any differences in the observed distributions should be entirely due to different amounts of angular momentum. As can be seen from Fig. 3, there are noticeable differences in the distributions. The $^4$He induced reaction gives results that resemble the triangular theoretical distribution more than the almost oval $^{16}$O induced distribution. This difference may also be seen on examining the moments of conditional distributions (Figs. 13, 15 and 17) which are sensitive to the general shape of the distributions. In all cases the $^4$He bombardment produces results that agree better with theory than the $^{16}$O bombardment. The conclusion is that qualitatively angular momentum is responsible for a general "washing out" of the predicted triangular shape of the distribution. It is also responsible for a broadening of the distribution, as can be seen from Fig. 7 and even more readily from Table I. The possibility that the differences between the two distributions are due to errors in measurements appears very unlikely. It can be seen from Table I that the differences in values of the overall widths are well outside experimental errors. The estimate of these errors was discussed in Section IV. One further possible source of error, restricted to the case of heavy-ion reactions and mentioned in Section II, is the loss of energy resolution with increases in beam intensity. The contribution from this effect was made insignificant by making measurements at several values of beam intensity, extrapolating energy widths to zero beam intensity and choosing a beam level for other runs (about 20 mAs) at which energy widths differed very little (less than ~1% in the variance of the distribution) from those at zero beam intensity.

The effects of angular momentum examined above are confirmed by comparing the reaction $^{182}$W + $^{16}$O = $^{198}$Pb with the reaction $^{209}$Bi + $^4$He = $^{213}$At. The two compound nuclei have almost identical values of the fissionability parameter, and the ranges of temperature involved are also similar. Comparison of Figs. 1 and 2, however, shows the Bi distributions to resemble their theoretical counterparts more than the equivalent W distributions. This is again reflected in the curves of first and second moments (Figs. 13,
15 and 17 compared with Figs. 12, 14 and 16). Furthermore, in the 102 MeV
\( ^{0}\text{16} \) and \( ^{18}\text{2} \) case the measured distribution compares fairly well with the
theoretical one, while in the 165 MeV bombarding energy case, the comparison
is poorer in all aspects. This difference is undoubtedly due to the angular
momentum involved, since it is much less significant over a comparable span
of nuclear temperature in the \( ^{4}\text{H} \) induced fission case.

As was mentioned earlier, the theory of Nix and Swiatecki is expected to
apply to the fission of elements lighter than radium (i.e., to cases for which
the fissionability parameter, \( x \) is \( \sim \leq 0.68 \)). One of the reasons for this
restriction is that above \( x \sim 0.68 \) the saddle-point shape no longer consists
of two well-defined fragments connected by a relatively thin neck, and thus,
cannot be approximated by two tangent spheroids.\(^1\) As angular momentum
increases, recent liquid-drop calculations indicate\(^1\) that the neck grows
thicker. Even at lower values of \( x \), the data may be outside the range
required for comparisons with theory due to the presence of a thick neck pro­
duced by large angular momentum. Reference \( ^{18} \) gives quantitative results on
the increase in thickness of the neck with angular momentum. It was found
that for the maximum angular momenta involved in the \( ^{17}\text{0} + ^{0}\text{16} \) bombardment the
neck was no thicker than that involved in the low energy \( ^{209}\text{Bi} + ^{4}\text{H} \) bombardi­
ments, in which agreements between experiment and theory were excellent. Thus
this effect of saddle-point neck thickening may possibly play a role, but does
not in itself explain all angular momentum effects.

VI. SUMMARY AND CONCLUSION

To summarize the comparisons presented above, the following factors should
be pointed out:

(1) In cases involving low angular momenta and low nuclear temperatures,
the agreement between experiment and theory is excellent. An examination of
the distribution resulting from the 80 MeV \( ^{4}\text{H} \) bombardment of \( ^{209}\text{Bi} \) in all
its aspects illustrates this point. The theoretical distribution is a very good
replica of the experimental distribution in every way.

(2) The dependence on temperature of the widths of distributions is
different from that predicted by the theory. This lack of agreement may be due
in part to pre-fission neutron evaporation. In the heavy-ion cases, where
agreement in temperature dependence is found, such agreement is likely to be fortuitous.

(3) Angular momentum effects, which have not been included in the theoretical development, tend to broaden the experimental $F(E_{T*}, A_1)$ distributions, and cause their contour representations to lose the predicted triangular shape.

To conclude, it must be stressed that the general agreement between theory and experiment is remarkably good, when we remember the restricted model which forms the basis of the theory. Not only does it reproduce reasonably well such gross features as the average total kinetic energy and the widths of mass-yield curves, but it predicts accurately the general triangular shape of the complete mass-total kinetic energy distributions. The only possibly serious shortcoming of the theory is the prediction concerning the temperature dependence of the widths. Even this problem may be due in part to an inadequate relation between the excitation energy and the nuclear temperature used throughout this work. We, therefore, consider the Nix-Swiatecki theory to be useful in providing a theoretical basis for fission data of elements lighter than radium. The theory does not restrict itself to mass-total kinetic energy distributions, and comparison with other types of data (e.g. excitation energies of fragments as reflected in their neutron emission distributions) would be extremely useful. It would also be desirable to evolve a similar theory that includes angular momentum effects, and one that is more realistic in adding a hyperbolic neck between the two spheroids when these are overlapping or tangent to each other, as in the case of saddle-point shapes. Preliminary work on this latter problem has been done by Nix and Swiatecki with encouraging results.
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APPENDIX I

Neutron Correction Formulae to the Moments of Experimental Conditional Distributions

The method used in deriving neutron-correction formulae to moments of measured distributions was based on the method of Terrell and that of Haines. The final equations differ somewhat from those of Haines primarily because higher order terms, which have a noticeable effect on the results, are retained.

In the following formulae when two subscripts are given, the first refers to the fragment number, the second to the sequential number of the neutron, the evaporation of which we are considering. Thus, for example, $E_{1j}$ and $A_{1j}$ are, respectively, the energy and the mass of fission fragment 1 after the evaporation of the j'th neutron (i.e., $A_{1j} = A_1 - j$). Applying vector analysis to the emission of the j'th neutron from fragment 1 at an angle $\theta_{1j}$ in the center-of-mass system of the moving fragment, the following expression is obtained:

$$E_{1j} = \frac{A_{1j} E_{1j-1}}{A_{1j-1}} + \frac{m \eta_{1j}}{A_{1j}} - 2 \left( \frac{m \eta_{1j} E_{1j-1}}{A_{1j-1}} \right) \cos \theta_{1j} \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots \cdots 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A. Correction to the Averages of Conditional Distributions
in Kinetic Energy

The correction to the average total kinetic energy for a given mass is obtained by successive application of expression (i). Neglecting terms of the order of \( m/A_1 \) and reducing, the following equation was obtained:

\[
\langle E_{T*} \rangle = \frac{A_1}{A_1} \langle E_1 \rangle + \frac{A_2}{A_2} \langle E_2 \rangle = \langle E_T \rangle \left( 1 - \frac{\nu A_2}{A_1 A_c} - \frac{\nu A_1}{A_2 A_c} \right)
\]

\( A_c \) is the mass of the compound nucleus, and the asterisk here, as in the main text, refers to a quantity uncorrected for neutron effects. Solving for \( \langle E_T \rangle \), we obtain the required correction to average total kinetic energy values at fixed values of the mass.

B. Correction to the Variances of the Conditional Distributions
in Total Kinetic Energy

The derivation of corrections to the variance of the conditional total kinetic energy distributions follows a similar pattern and is also based on the successive application of recursion relation (i). In this derivation, terms of order \( m/A_c \) are retained, while higher order terms are not. Thus, recalling the definition of a variance,

\[
\mu_2(E_{T*}) = \langle E_{T*}^2 \rangle - \langle E_{T*} \rangle^2
\]

and the relationships,

\[
E_{T*} = E_{1y} + E_{2y}
\]

and

\[
\langle E_{T*} \rangle = \langle E_{1y} \rangle + \langle E_{2y} \rangle
\]

we obtain

\[
\mu_2(E_{T*}) = \mu_2(E_{1y}) + \mu_2(E_{2y}) + 2 \left\{ \langle E_{1y} E_{2y} \rangle - \langle E_{1y} \rangle \langle E_{2y} \rangle \right\}
\]

It can be shown that, with proper use of expression (i) and the assumptions discussed above, together with some lengthy but straightforward algebra, evaluating the above expression term by term, the following equation may be obtained:
The further assumption used in the development of the above equation was that there is no correlation between the kinetic energies of successive neutrons emitted from the same fragment. Solving the above equation for \( \mu_2(\mathcal{E}_T) \) gives the corrected variance of the \( \mathcal{E}_T \) distribution at a given mass in terms of the uncorrected variance.

### C. Correction to the Variances of the Conditional Distributions in Mass

The calculation of the correction to the mass distribution variance for a given total kinetic energy is complicated by the manner in which the masses were calculated from the energy data (see main text). In this work measured masses are given by

\[
A_2 = \frac{E_1^* A_c}{E_T^*},
\]

from which it can be shown that

\[
\mu_2^*(A_1) = \frac{A_c^2}{E_T^* \mu_2(\mathcal{E}_1^*)}.
\]

Thus, it was necessary to evaluate \( \mu_2(\mathcal{E}_1^*) \) for constant values of \( E_1^* \). This was done by using the recursion relation (1) to evaluate \( E_1^* \) as a function of \( E_1 \). The expression \( E_1 = A_2 E_T/A_c \) was then applied, where \( E_T \) was given (also through the recursion relation) by:

\[
E_T^{*} = E_{T}^{*} \left[ 1 + \frac{\nu A_2}{A_1 A_c} + \frac{\nu A_1}{A_2 A_c} - 2 \left( \frac{m \eta_1^2 A_2}{A_c E_T^* A_1} \right) \frac{1}{2} \sum_{i=1}^{V} \cos \theta_{1i} - 2 \left( \frac{m \eta_2^2 A_1}{A_c E_T^* A_2} \right) \frac{1}{2} \sum_{j=1}^{V} \cos \theta_{2j} \right].
\]

Thus a complete expression for \( E_1^* \) expressed in terms of required quantities was available, and its variance could be calculated by first calculating \( \langle E_1^{*2} \rangle \) and \( \langle E_1^* \rangle^2 \). Since the mass distributions are symmetric, we have

\[
\langle A_1/A_c \rangle = \frac{1}{2} \quad \text{and} \quad \mu_2(A_1) = \langle (A_1/A_c)^2 \rangle - \frac{1}{4}.
\]
Combining this with the above results and performing a considerable amount of algebra, the final expression obtained is:

\[ \mu_2^*(A_2) = \mu_2(A_2) \left( 1 - \frac{h\nu}{A_c} \right) + 2\nu m_{A_c} \frac{\langle \eta \rangle}{E_T^*} \]

The solution of this equation for \( \mu_2^*(A_2) \) gives the required corrected expression in terms of the measured uncorrected variance. The further assumption made in this last derivation was that there is no correlation between angles of emission of successive neutrons.

The value of \( \nu \) (the average number of neutrons evaporated from a fragment) which was required in the above derivations was estimated by means of the following energy-balance expression:

\[ E_x + \langle E_R \rangle = \langle E_T \rangle + \langle E_y \rangle + 2\nu (\langle B_n \rangle + \langle \eta \rangle) \]

In this expression, \( \langle E_R \rangle \) is the average energy released during the fission process (averaged over all masses) as calculated from a computer program of Milton, \( E_x \) is the total excitation energy of the fissioning compound nucleus (obtained from a knowledge of the bombarding energy and the masses of the nuclei involved), \( \langle B_n \rangle \) is the average neutron binding energy (also averaged over all masses and obtained from the program of Milton) and \( \langle E_y \rangle \) is the average energy associated with the emission of \( \gamma \)-rays from the fragments. Since \( \langle E_y \rangle \) is not known for the systems studied in this work, the value for the case of californium of 9 MeV was used. \( \langle \eta \rangle \), the average kinetic energy of the neutrons, was calculated from:

\[ \langle \eta \rangle = \frac{4}{3} \langle \text{fragment nuclear temperature} \rangle = \frac{4}{3} \sqrt{\frac{8\langle X_1 \rangle}{A_1}} \]

where \( \langle X_1 \rangle \) is the average fragment excitation energy. For the purpose of these calculations, \( \langle X_1 \rangle \) was taken to be \( \frac{4}{3}(\langle E_R \rangle + E_x - \langle E_T \rangle) \).
APPENDIX II

Theoretical Energy Mass Distributions Which Include Prompt Neutron Evaporation Effects

An alternative method for approaching the problem of prompt neutron emission from fission fragments is to include this effect in the theoretical development and obtain distributions that compare directly with measured distributions in every way except for angular momentum effects. Such an approach was possible because Nix and Swiatecki \(^3\) have obtained expressions not only for mass-kinetic energy distributions, \(P(E_T, A_\perp)\), but also for mass-kinetic energy excitation-energy distributions, \(P(E_T, A_\perp, X)\). \((X_\perp\) is the excitation energy of fragment 1 associated with the collective vibrations and deformations of the fragment.) These latter distributions are given by Nix and Swiatecki only in the lowest order of approximation, which, however, is satisfactory for the purpose of neutron correction.

The following numerical method was used to transform the initial \(P(E_T, A_\perp)\) distributions to corrected \(P(E_T^*, A_\perp)\) distributions. The theoretical mass-total kinetic energy distribution \(P(E_T, A_\perp)\) was divided into unit areas \(\Delta E_T\) by \(\Delta A_\perp\), where \(\Delta E_T = 2\) MeV and \(\Delta A_\perp = 1\) amu. \(P(E_T, A_\perp)\) was evaluated at the centers of these unit areas. Thus each unit area was characterized by a combination of \(E_T\) and \(A_\perp\) values, a statistical weight given by the value of \(P(E_T, A_\perp)\) at the center of it, and by its own probability distribution \(P(X_\perp)\) in the excitation energy of fragment 1. The distribution \(P(X_\perp)\) associated with energy unit \(\Delta E_T\Delta A_\perp\) area was calculated from the lowest order expression for \(P(E_T, A_\perp, X_\perp)\) of Nix and Swiatecki. The probability was evaluated at the centers of differential units of \(\Delta X_\perp\), the size of which was left adjustable so that the whole \(P(X_\perp)\) distribution was adequately described in every case. Thus, unit volumes of dimensions \(\Delta E_T\) by \(\Delta A_\perp\) by \(\Delta X_\perp\) were considered, each with a characteristic combination of \(E_T, A_\perp\) and \(X_\perp\) and a statistical weight obtained from evaluating \(P(E_T, A_\perp)\) and \(P(X_\perp)\) at this combination. It was necessary to evaluate the two probabilities \(P(E_T, A_\perp)\) and \(P(X_\perp)\) separately rather than directly from the \(P(E_T, A_\perp, X_\perp)\) expression because the accuracy required in the \(E_T\) vs \(A_\perp\) distribution was one of second order approximation, while the available \(P(E_T, A_\perp, X_\perp)\) expression is one of first order. By means of energy balance considerations and the theory of Nix and Swiatecki, it is possible to calculate the corresponding \(X_\perp\) for any given value of \(X_\perp\). The
Following equation was then applied:

\[ E_X + E_R = H_T + E_T + X_1 + X_2 \]

This relationship balances the total energy available, consisting of \( E_X \), the total excitation energy of the compound nucleus and of \( E_R \), the total energy released in the fission process, against the way in which it is distributed to the fragments (\( X_1 \) and \( X_2 \) are excitation energies due to collective motions of the fragments and \( H_T \) is the total internal excitation energy that the fragments possess). \( E_X \) and \( E_R \) are both obtained from nuclear mass tables. \(^{21}\) \( E_R \) is a function of \( A_1 \) and was calculated by means of a computer program of Milton. \(^{26}\) The above equation thus gives a value for \( H_T \) for any particular unit \( \Delta E_T \Delta A_1 \Delta X_1 \) volume. \( H_T \) and \( E_T \) were divided between the two fragments; \( H_T \) was divided according to \( A_1/A_2 = H_1/H_2 \) and \( E_T \) according to the momentum conservation relationship \( E_1/E_2 = A_2/A_1 \). Thus, for any given unit volume, the kinetic energies of both fragments, \( E_1 \) and \( E_2 \), and the total excitation energies of both fragments \( X_1 \) and \( X_2 \) (where \( X_1 = X_1 + H_1 \)) are known, and the numbers of neutrons evaporated may be obtained.

For each unit volume, the random evaporation of neutrons from both fragments was now considered. Two recursion relations were used for this purpose. The first relates the excitation energy \( X_{1j} \) of fragment 1 after the emission of the \( j \)th neutron to that before the neutron emission

\[ X_{1j} = X_{1j-1} - \langle B_1(A_1) \rangle - \eta_{1j} \]

where \( \langle B_1(A_1) \rangle \) is the average neutron binding energy for fragment 1. \( \langle B_1(A_1) \rangle \) is a function of the mass split and is averaged over the fragment charge distribution; it is calculated by the program of Milton. \(^{26}\) \( \eta_{1j} \) is the kinetic energy of the \( j \)'th neutron and is given by

\[ \eta_{1j} = 2 \sqrt{\frac{8 X_{1j-1}}{A_{1j-1}}} \]

The neutron evaporation process for fragment 1 is terminated when the following condition holds:

\[ X_{1j-1} < \langle B_1(A_1) \rangle - \eta_{1j} \]
The second recursion relation is given by equation (i) of Appendix I. It relates the kinetic energy before neutron emission to that after neutron emission for fragment 1. Analogous relationships hold for fragment 2. The assumptions of Appendix I concerning the isotropic emission of neutrons in the center-of-mass system and the absence of correlations between successive neutrons were also made in this method. Thus the value of \( \cos \theta_{1j} \) in equation (i) of Appendix I was selected by a random number generator between the limits \(-1 \leq \cos \theta_{1j} \leq 1\).

By means of successive application of the above two recursion relations, \( E_1 \) and \( E_2 \) values of any unit \( \Delta E_{T}, \Delta A_1, \Delta X_1 \) volume were transformed to post-neutron \( E_1^* \) and \( E_2^* \) values. These were then treated exactly as the measured energies, given \( E_{T}^* = E_1^* + E_2^* \) and \( A_1 = (E_2^*A_c)/E_{T}^* \). For any unit volume, this statistical random number process was repeated \( n \)-times, \( n \) being the same for all unit volumes of any particular calculation. As \( n \) increased, the statistical accuracy of this method increased. A new distribution, \( P(E_{T}^*, A_1) \), was generated from the above results as follows. Each unit volume contributed \( n \)-times to this new distribution, and the extent of the contribution of the unit volume was determined by its statistical weight mentioned above. The procedure of using differential volumes, characterized by values of \( E_{T}, A_1 \) and \( X_1 \) and by statistical weights due to the distributions \( P(E_{T}, A_1) \) and \( P(X_1) \) to give contributions to a probability distribution, \( P(E_{T}^*, A_1) \), which has, as coordinates, only the total kinetic energy and mass, is equivalent to a numerical integration over \( X_1 \). The new distribution was normalized to the old distribution.

The accuracy of the calculation was governed by \( n \), the number of times it was repeated for each unit volume, and by the accuracy of the numerical integration over \( X_1 \). Both effects were studied, and reproducibility (for different values of \( n \) and different accuracies of the numerical integration) to an accuracy of 0.5% in the moments of the mass-yield and energy-yield distributions was required. The statistical scatter in the yield distributions and in the moments of conditional distributions was greatly reduced as \( n \) was increased. The highest value of \( n \) used was 20. Higher values were impractical due to the large amount of computer time required. The scatter in the calculated points is greater in the case of moments of the conditional total kinetic energy distributions, taken as a function of mass, than in the case of the moments of conditional mass distributions taken as a function of total kinetic energy.
This is in accordance with expectations since the neutron evaporation perturbs the total kinetic energy much more than it does the mass, when the latter is obtained in the manner described in this work.

Figure 18 shows the results for the reaction of $^{182}W$ with $^{4}\text{He}$ ($n = 20$). It can be seen, that since the experimental distributions were narrower than the uncorrected theoretical ones, the correction due to neutron effects does not help the agreement as far as the width is concerned. The agreement between the shapes of the theoretical and experimental distributions, however, is enhanced by including neutron effects in the theoretical distribution. This is reflected in the cases of the $\mu_2(A_T) vs E_T$ and $(E_T)$ vs mass plots and also in the case of $\mu_2(E_T)$ vs mass, if the difference in magnitude is neglected and only the shape of the curve is considered. Table II gives comparative values of moments of the overall distributions (for the $^{182}W + ^4\text{He}$ case) for the two methods of neutron correction.
FOOTNOTES AND REFERENCES

* This work was done under the auspices of the U.S. Atomic Energy Commission.
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‡ Present address: California Institute of Technology, Pasadena, California.
†† On leave from, and now at Los Alamos Scientific Laboratory, Los Alamos, New Mexico.

16. The full width at half maximum, FWHM, is given, for a Gaussian distribution, by: 
   \[
   \text{FWHM} = 2.36 \sqrt{\mu_2}
   \]
22. A. E. S. Green, Phys. Rev. 95, 1006 (1954).
24. The fissionability parameter $x$ may be defined by:

$$ x = \frac{E^0_c}{2E^0_s}, $$

where $E^0_c$ and $E^0_s$ are the Coulomb and surface energies of a sphere, respectively. This definition is equivalent to the following alternative definition:

$$ x = \frac{(Z^2/A)_{\text{crit}}}{(Z^2/A)}. $$

The value for $(Z^2/A)_{\text{crit}}$ of 50.13 is usually found in the literature. Recent experiments, however, indicate that a better value for $(Z^2/A)_{\text{crit}}$ is 48.4. When comparisons are made with the theory of Nix and Swiatecki, the old value of 50.13 was retained so that the set of nuclear constants used throughout their work and this paper form a self-consistent set.
Table I. Experimental results and theoretical calculations for the moments of overall distributions for all reactions studied. Experimental results corrected for prompt neutron effects are also given. The errors shown are estimates of systematic errors (see text). Statistical errors are small in comparison with systematic errors. Certain duplicated experiments are also shown. \( E_{\gamma} \) and \( \theta \) are the bombarding energy and the nuclear temperature at the saddle respectively. \( \langle E_T \rangle \) is the average total kinetic energy and \( \sigma^2 \langle E_T \rangle \) the variance of the overall total kinetic energy-yield distributions. \( \sigma^2 \langle A_1 \rangle \) is the variance of the overall mass-yield distribution. The asterisk superscript characterizes values after the emission of prompt neutrons.

<table>
<thead>
<tr>
<th>Reaction</th>
<th>( E_{\gamma} ) (MeV)</th>
<th>( \theta ) (MeV)</th>
<th>Number of Events (x103)</th>
<th>Experiment ( \langle E_T \rangle ) (MeV)</th>
<th>Theory ( \langle E_T \rangle ) (MeV)</th>
<th>Uncorrected</th>
<th>Corrected</th>
<th>Experiment ( \sigma^2 \langle E_T \rangle ) (MeV)²</th>
<th>Theory ( \sigma^2 \langle E_T \rangle ) (MeV)²</th>
<th>Uncorrected</th>
<th>Corrected</th>
<th>Experiment ( \sigma^2 \langle A_1 \rangle ) (amu)²</th>
<th>Theory ( \sigma^2 \langle A_1 \rangle ) (amu)²</th>
</tr>
</thead>
<tbody>
<tr>
<td>( \text{Bi}^{209} + \text{He}^4 \rightarrow \text{Te}^{133} )</td>
<td>120</td>
<td>1.87</td>
<td>197</td>
<td>14113 ± 1244</td>
<td>149</td>
<td>102 ± 26</td>
<td>78</td>
<td>108 ± 18</td>
<td>179 ± 27</td>
<td>169 ± 20</td>
<td>120 ± 16</td>
<td>191 ± 20</td>
<td>165 ± 14</td>
</tr>
<tr>
<td>( \text{Au}^{197} + \text{He}^4 \rightarrow \text{Te}^{131} )</td>
<td>120</td>
<td>1.95</td>
<td>132</td>
<td>1352 ± 1314</td>
<td>131</td>
<td>91 ± 16</td>
<td>67</td>
<td>105 ± 15</td>
<td>192 ± 26</td>
<td>166 ± 21</td>
<td>120 ± 16</td>
<td>180 ± 23</td>
<td>162 ± 18</td>
</tr>
<tr>
<td>( \text{W}^{182} + \text{He}^4 \rightarrow \text{Os}^{106} )</td>
<td>120</td>
<td>2.00</td>
<td>145</td>
<td>1222 ± 1284</td>
<td>130</td>
<td>86 ± 16</td>
<td>68</td>
<td>101 ± 14</td>
<td>220 ± 27</td>
<td>204 ± 22</td>
<td>120 ± 16</td>
<td>180 ± 23</td>
<td>162 ± 18</td>
</tr>
<tr>
<td>( \text{U}^{238} + \text{O}^{16} \rightarrow \text{Pu}^{198} )</td>
<td>165</td>
<td>2.07</td>
<td>108</td>
<td>1402 ± 1374</td>
<td>142</td>
<td>13 ± 48</td>
<td>134</td>
<td>114 ± 23</td>
<td>256 ± 120</td>
<td>213 ± 20</td>
<td>165 ± 20</td>
<td>191 ± 23</td>
<td>171 ± 19</td>
</tr>
<tr>
<td>( \text{Er}^{170} + \text{O}^{16} \rightarrow \text{Os}^{106} )</td>
<td>165</td>
<td>2.04</td>
<td>159</td>
<td>1204 ± 1274</td>
<td>130</td>
<td>104 ± 110</td>
<td>106</td>
<td>104 ± 21</td>
<td>250 ± 22</td>
<td>235 ± 21</td>
<td>165 ± 20</td>
<td>191 ± 23</td>
<td>171 ± 19</td>
</tr>
<tr>
<td>( \text{Yb}^{174} + \text{O}^{16} \rightarrow \text{Os}^{106} )</td>
<td>125</td>
<td>1.70</td>
<td>31</td>
<td>125 ± 1295</td>
<td>130</td>
<td>133 ± 12</td>
<td>104</td>
<td>96 ± 14</td>
<td>217 ± 16</td>
<td>211 ± 22</td>
<td>125 ± 16</td>
<td>159 ± 23</td>
<td>131 ± 19</td>
</tr>
<tr>
<td>( \text{Lu}^{176} + \text{O}^{16} \rightarrow \text{Os}^{106} )</td>
<td>125</td>
<td>1.53</td>
<td>21</td>
<td>125 ± 127</td>
<td>130</td>
<td>122 ± 9</td>
<td>94</td>
<td>76 ± 10</td>
<td>190 ± 23</td>
<td>185 ± 19</td>
<td>125 ± 16</td>
<td>159 ± 23</td>
<td>131 ± 19</td>
</tr>
</tbody>
</table>
Table II. Comparison of the methods of correction for prompt neutron evaporation effects. The data refer to the fission of Os$^{186}$ as produced by a He$^+$ bombardment of W$^{182}$ at 120 MeV. The method of data correction is given in Appendix I, while the method of correction of theoretical calculations is given in Appendix II. The description of the moments tabulated is given in the caption of Table I.

<table>
<thead>
<tr>
<th></th>
<th>Experiment Uncorrected</th>
<th>Theory Uncorrected</th>
<th>Theory Corrected</th>
<th>Experiment Corrected</th>
</tr>
</thead>
<tbody>
<tr>
<td>$\langle E_T \rangle$ (MeV)</td>
<td>122</td>
<td>124</td>
<td>130</td>
<td>128</td>
</tr>
<tr>
<td>$\mu_2(E_T)(\text{MeV})^2$</td>
<td>86</td>
<td>138</td>
<td>101</td>
<td>68</td>
</tr>
<tr>
<td>$\mu_2(A_1)(\text{amu})^2$</td>
<td>220</td>
<td>278</td>
<td>256</td>
<td>204</td>
</tr>
</tbody>
</table>
FIGURE CAPTIONS

Fig. 1. Experimental and theoretical contour diagrams for the probability distributions, \( P(E_T, A_1) \), of a fragment total kinetic energy, \( E_T \), and mass, \( A_1 \), for the reaction \( \text{He}^4 + \text{Bi}^{209} \rightarrow \text{At}^{213} \rightarrow \text{fission} \). Several values of the nuclear temperature of the compound nucleus, \( \theta \), and corresponding laboratory bombarding energies, \( E_L \), are shown. The labels on the lines of constant probability have the following significance: the contour labeled 10, for example, passes through those regions of the \( E_T \) vs \( A_1 \) plane where an area of 6 MeV by 3 amu contains 1% of the total number of events. Seven contours are shown at all values of \( \theta \); higher contours are present in the case of narrow distributions at low \( \theta \) values, but are not shown.

Fig. 2. Experimental and theoretical contour diagrams of the mass-total kinetic energy probability distributions for the fission of \( \text{Pb}^{198} \) produced by \( ^{16} \text{O} \) bombardment of \( ^{182} \text{W} \) at two values of the nuclear temperature, \( \theta \), and bombarding energy, \( E_L \). The significance of contour labels is the same as that in Fig. 1.

Fig. 3. Experimental and theoretical contour diagrams of the mass-total kinetic energy distributions for the fission of \( \text{Os}^{186} \) at a nuclear temperature of 2 MeV. The \( \text{Os}^{186} \) compound nucleus was produced by a \( \text{He}^4 \) bombardment (at 120 MeV) of \( ^{182} \text{W} \) and by an \( ^{16} \text{O} \) bombardment (at 165 MeV) of \( ^{170} \text{Er} \). The significance of contour labels is the same as that in Fig. 1.

Fig. 4. Mass-yield and total kinetic energy-yield distributions (experimental and theoretical) for the fission of the \( \text{At}^{213} \) compound nucleus produced by \( \text{He}^4 \) bombardments of \( \text{Bi}^{209} \) at several bombarding energies. The units of yield are arbitrary. The \( E_T^* \) scale given is that for the \( \theta = 0.71 \) MeV case. Other experimental energy-yield distributions shown were normalized in such a way as to make their average total kinetic energy \( \langle E_T \rangle \), equal to \( \langle E_T \rangle \) of the \( \theta = 0.71 \) MeV distribution.

Fig. 5. Theoretical and experimental mass-yield and energy-yield distributions for the fission of \( \text{Tl}^{201} \) produced by bombardments of \( ^{197} \text{Au} \) with \( \text{He}^4 \) ions at two different energies. The units of yield are arbitrary, and the \( E_T^* \) scale refers to the \( \theta = 1.2 \) MeV case.
Fig. 6. Theoretical and experimental mass-yield and energy-yield distributions for the fission of $^{198}\text{Pb}$ produced by bombardments of $^{182}\text{W}$ with $^{16}\text{O}$ ions at two different energies. The units of yield are arbitrary, and the $E_{T}^*$ scale refers to the $\theta = 1.37$ MeV case.

Fig. 7. Theoretical and experimental mass-yield and energy-yield distributions for the fission of $^{186}\text{Os}$ at a nuclear temperature of 2 MeV. The $^{186}\text{Os}$ compound nucleus was produced by an $^{16}\text{O}$ and a $^{4}\text{He}$ bombardment. The units of yield are arbitrary.

Fig. 8. Variances of the overall total kinetic energy distributions, $\mu_{2}(E_{T})$, as a function of the nuclear temperature $\theta$, for several compound nuclei. The open triangles in the $^{186}\text{Os}$ case refer to the reaction $^{174}\text{Yb} + ^{12}\text{C} = ^{186}\text{Os}$. The open squares refer to $^{170}\text{Er} + ^{16}\text{O} = ^{186}\text{Os}$, while the closed squares refer to $^{182}\text{W} + ^{4}\text{He} = ^{186}\text{Os}$. The $^{198}\text{Pb}$ was produced by $^{16}\text{O}$ bombardments of $^{182}\text{W}$. The $^{197}\text{Tl}$ and $^{209}\text{At}$ were obtained by $^{4}\text{He}$ bombardments of $^{197}\text{Au}$ and $^{209}\text{Bi}$, respectively. The different symbols in these two cases represent different experiments. The solid line shows the theoretical result. The experimental points have been corrected for neutron emission effects. The size of the symbols is not to be taken as representative of the errors involved. Estimated errors are tabulated in Table I.

Fig. 9. Variances of the overall mass-yield distributions, $\mu_{2}(A_{1})$, as a function of the nuclear temperature $\theta$. The symbols have the same meaning as in Fig. 8. The solid line gives the theoretical calculations. The experimental results have been corrected for prompt neutron emission effects. The size of the symbols is not representative of the errors in measurement.

Fig. 10. Variances of the overall total kinetic energy distributions as a function of the nuclear temperature $\theta$. Identical to Fig. 8, but experimental results have not been corrected for neutron evaporation effects.

Fig. 11. Variances of the overall mass-yield distributions as a function of the nuclear temperature $\theta$. Identical to Fig. 9, but experimental results have not been corrected for neutron evaporation effects.
Fig. 12. Average total kinetic energy $\langle E_T \rangle$, as a function of mass for the fission of At$^{213}$. The solid curves give the theoretical results, the closed circles the experimental results at three values of $\theta$. The experimental results are corrected for neutron evaporation effects.

Fig. 13. Average total kinetic energy $\langle E_T \rangle$, as a function of fragment mass for the cases of $\text{W}^{182} + \text{He}^4 = \text{Pb}^{198}$ (at two bombarding energies), $\text{W}^{182} + \text{He}^4 = \text{Os}^{186}$ and $\text{Er}^{170} + \text{O}^{16} = \text{Os}^{186}$. The solid curves give the theoretical results. The closed circles give experimental results corrected for neutron evaporation effects.

Fig. 14. Variances of the conditional total kinetic energy distributions, $\mu_2(E_T)$, as a function of mass for the case of the fission of At$^{213}$. The solid lines give the theoretical results; the closed circles give experimental results not corrected for neutron effects.

Fig. 15. Variances of the conditional total kinetic energy distributions, $\mu_2(E_T)$, as a function of mass for the cases of the fission of Pb$^{198}$ and Os$^{186}$. The solid lines give the theoretical calculations. The closed circles give experimental results not corrected for neutron effects.

Fig. 16. Variances of conditional mass distributions, $\mu_2(A_1)$, as a function of the total kinetic energy, $E_T$, for the case of $\text{He}^4 + \text{Bi}^{209} = \text{At}^{213} \rightarrow \text{fission}$. The solid curves give theoretical results. The closed circles give experimental results not corrected for prompt neutron evaporation effects.

Fig. 17. Variances of conditional mass distributions, $\mu_2(A_1)$, as a function of the total kinetic energy, $E_T$, for the cases of the compound nuclei Pb$^{198}$ and Os$^{186}$. The solid curves give theoretical results, and the closed circles give experimental results not corrected for neutron evaporation effects.

Fig. 18. Mass and total kinetic energy-yield distributions and moments of conditional distributions for the reaction $\text{W}^{182} + \text{He}^4 = \text{Os}^{186} \rightarrow \text{fission}$ at a He$^4$ energy of 120 MeV. The solid curves give the original theoretical distributions, the open circles the theoretical distributions which include neutron effects and the closed circles the experimental distributions not corrected for neutron effects. The labels on the axes and ordinates have the same meaning as those in the corresponding earlier figures that refer to the same reaction, but in which neutron corrections to the theoretical distributions are not included.
Fig. 1
Fig. 2
Experiment (a) Experiment (b)

\[ \text{He}^4 + \text{He} = \text{Er}^{170} + \text{O}^{186} \]

Fig. 3
Fig. 4
Fig. 5
Fig. 6
Fig. 7
Fig. 8
Fig. 9
Fig. 10
Fig. 11
Fig. 12

\[
\langle E_T \rangle \text{ (MeV)}
\]

- \( \theta = 0.71 \text{ MeV} \)
  - \( E_L = 40 \text{ MeV} \)

- \( \theta = 1.42 \text{ MeV} \)
  - \( E_L = 80 \text{ MeV} \)

- \( \theta = 1.87 \text{ MeV} \)
  - \( E_L = 120 \text{ MeV} \)

Mass (amu)

Fig. 42
Fig. 13

\[ W^{182} + O^{16} = Pb^{198} \]
\[ E_L = 102 \text{ MeV} \]
\[ \theta = 1.4 \text{ MeV} \]

\[ W^{182} + O^{16} = Pb^{198} \]
\[ E_L = 165 \text{ MeV} \]
\[ \theta = 2.1 \text{ MeV} \]

\[ W^{182} + He^4 = Os^{186} \]
\[ E_L = 120 \text{ MeV} \]
\[ \theta = 2.0 \text{ MeV} \]

\[ Er^{170} + O^{16} = Os^{186} \]
\[ E_L = 165 \text{ MeV} \]
\[ \theta = 2.0 \text{ MeV} \]
Fig. 14
Fig. 16

\[ \mu_2(A_1)^2 \text{ (amu)} \]

\[ E_L = 40 \text{ MeV} \]

\[ \theta = 0.71 \text{ MeV} \]

\[ E_L = 80 \text{ MeV} \]

\[ \theta = 1.42 \text{ MeV} \]

\[ E_L = 120 \text{ MeV} \]

\[ \theta = 1.87 \text{ MeV} \]
Fig. 17
Fig. 18
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