Ion Diffusion Within Water Films in Unsaturated Porous Media

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1. INTRODUCTION

The mobility of dissolved ions through the aqueous phase in soils and geological materials is important in a wide variety of processes including nutrient transport to plant roots and soil microorganisms,1,2 the performance of barriers for subsurface waste isolation,3,4 and electrical resistivity measurements employed in geophysical mapping of the subsurface.5–7 Interest in these processes has motivated a large number of studies on diffusion of solutes in unsaturated as well as saturated soils and geological media, summarized in comprehensive reviews.8–11

The effective diffusion coefficient of a solute of interest in porous media, \(D_e\), is of central importance in these numerous investigations, linking macroscopic diffusive fluxes, \(J\), to gradients in their aqueous concentrations, \(C\). For diffusion in response to a concentration gradient along the \(x\)-axis, Fick’s Law gives \(J\) as

\[
J = -D_e \frac{dC}{dx}
\]  

(1)

The magnitude of \(D_e\) depends on the diffusion coefficient of the species of interest in bulk water \(D_w\), porosity \(n\), volumetric water content \(\theta\), and tortuosity factor \(\tau_o\). Recognition of the controlling influence exerted by volumetric water content \(\theta\) (the product of porosity \(n\) times water saturation \(S\)) and water film continuity goes back to early studies of solute diffusion in soils.12–14 The pore network generally constrains solutes to diffuse along paths with effective lengths \(l_e\), that are longer than the bulk diffusion length \(l_b\) (Figure 1a), and these paths become longer as \(\theta\) decreases (Figures 1b, c). Various definitions of tortuosity exist,15 and here we use one convention of equating \(\tau_o\) with \((l_e/l_b)^2\) such that \(\tau_o\) decreases as \(\theta\) decreases.12,16

Diffusion within soils and geologic materials is sometimes further described as occurring not only through the aqueous phase in pores, but also via surface diffusion paths along water-mineral interfaces17 (Figure 1d). Explanations for decreased magnitudes of \(D_e\) at low water contents include the constrictivity of very narrow paths, interactions with mineral surfaces, and increased water viscosity near these surfaces. These effects have also been included in models of diffusion in porous media.12,18,19 While many porosity-saturation-tortuosity-constrictivity models have been developed to predict \(D_e\), independent quantification of individual factors is challenging. For simplicity, we will use the convention of expressing \(D_e\) as a reduction of \(D_w\) through two factors, \(\theta\) and \(\tau_o\)

\[
D_e = \beta D_w
\]  

(2)

Thus, the impedance factor \(\beta\) is equal to \(D_w/(\theta \tau_o)\) and ranges from unity (for the limiting case of microscopically straight pathways with bulk fluid properties), down to zero (when solutes are immobilized through sorption and/or disconnected aqueous phases). \(D_e\) will be used later to assess the collective significance of all other factors besides \(\theta\) (e.g., \(\tau_o\)).

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constrictivity, potentially increased viscosity, and increased interactions with interfaces) that contribute to decreased ion mobility as water saturation becomes very low.

It is worth noting for later discussion that the ratio $D_\theta/(\theta D_o) \approx f$ is the inverse of Saripalli et al.’s diffusion tortuosity factor $\tau_s$, defined as the ratio of the air−water interfacial area in the unsaturated porous medium ($a_{aw}$) relative to that of an equivalent bundle of capillary tubes ($a_{aw,o}$). From the conceptual model presented in Figure 1, it is clear that the air−water interfacial area approaches the specific surface area of the solid phase at very low $\theta$. Thus, at very low $\theta$, $f$ can be compared with the inverse of Saripalli et al.’s $\tau_s$ with the air−water interfacial area equated with the specific surface area of the solid phase.

The vast majority of solute diffusion studies have been conducted in porous media at intermediate to high $\theta$, typically in the range of about 0.1−0.5, which represent most soil and sediment environments. Some $D_\theta$ measurements at $\theta < 0.1$ are available in the literature, and low water saturations are common in (semi-) arid region soils and some deeper geologic formations including oil, gas, and geothermal reservoirs. In addition to their relevance in drier environments, measurements of $D_\theta$ at low $\theta$ are needed for basic understanding of limiting conditions that allow transport via diffusion through the wetting fluid phase in unsaturated porous media, including the percolation threshold $\theta_{bh}$ needed to permit diffusive transport. Although models for solute diffusion can be categorized into those that explicitly allow diffusion coefficients to become infinitesimally small as water saturation approaches zero, and those that consider a percolation threshold, the lower limits of diffusion remain unclear.

Thinning of adsorbed water films has been invoked as the determinant for the lower limit of diffusion for ionic solutes because of their hydration and confinement between solid−water and water−gas interfaces. This limit is expected when water film thicknesses approach dimensions of hydrated ion diameters. Given effective radii of ion hydration typically ranging from about 0.25−0.5 nm, their diffusion appears feasible within water films at least as thin as 1 nm. Further constraints on ion mobility may result from strong interactions and ordering of water at mineral surfaces inferred from vapor adsorption energies, surfaces, spectroscopic measurements, and molecular dynamics (MD) simulations. Indeed, the effective viscosity of water within the first two layers of the mineral surfaces has long been hypothesized to reduce ion mobility. However, quasi-elastic neutron scattering measurements and other MD simulations indicate that mobilities of water and ions approach their bulk solution values rapidly beyond the first monolayer away from solid surfaces.

Experimental tests of water and ion mobility along mineral water interfaces have typically been done in systems with moderate to high surface area. The strong influence of surface area on the $\theta_{bh}$ needed for diffusion has been well documented. However, in order to isolate diffusion along adsorbed water films, it is useful to conduct studies in low $\theta$ systems where the complicating influences from water retained within clay interlayers and in intragranular pores are absent. To our knowledge, such experiments have not previously been conducted. Thus, this study focuses on solute diffusion in homogeneous quartz sands at low $\theta$.

Examination of the lower limit of solute diffusion and its relation to water film thickness introduces several challenges in measurements and analyses. Tests require high spatial resolution or long experimental times in order to explore lower limits of diffusive transport. Moreover, for purposes of uniquely identifying the controlling role of adsorbed films, the relative fraction of water retained in intragranular pores and clay interlayers needs to be very small. These considerations led us to conduct unsaturated diffusion measurements on monodisperse quartz sands, conceptually illustrated in Figure 1. The required spatial resolution for measuring diffusion profiles was achieved through using a synchrotron X-ray fluorescence microprobe. Because of difficulties in homogeneously packing the sands, many of the diffusion profiles were found to be rather irregular and therefore best analyzed through inverse modeling.

Figure 1. Conceptual illustrations of how solute diffusion pathways become more tortuous as the water content is decreased. Panels a−c show increased tortuosity in traversing multiple pores, with the greatest increases in path lengths expected during initial drainage, rather than with film thinning. Panels d−f show hypothetical diffusion pathways in bulk pore water (yellow) and along mineral surfaces (red), emphasizing the controlling role of water films when water saturation is low.
2. MATERIALS AND METHODS

2.1. Sands. High purity quartz sands (total impurities <22 ppm) were obtained from the Quartz Corporation (Spruce Pine, NC). These sands were sieved to retain the 106–125 μm grain size fraction for use in the diffusion experiments. Specific surface areas determined by Kr-BET (Quantachrome Autosorb-1) were 0.069 ± 0.002 m² g⁻¹, about 3.5 times greater than that of 110 μm diameter spheres of equivalent quartz density (2.65 g cm⁻³).

2.2. Diffusion Cells and Sand Packing. The general approach used in all experiments was the half-cell method, involving joining a sample containing the diffusion tracer (source half) to an identical sample initially lacking the tracer (sink half), then measuring concentration distributions along the joined system at a later time using a synchrotron X-ray fluorescence microprobe. To facilitate accurate location of the interface between the two halves (x = 0) with the X-ray microprobe, anatase (TiO₂) powder was mixed into the source sand at 2.0 mg g⁻¹ as a stationary label. RbBr was used as the diffusing tracer, initially present only in the source half. Either CsI or KI was added uniformly to both source and sink sands to provide a higher background concentration of relatively nonreactive ions in which Rb⁺ and Br⁻ diffused. Experiments were conducted over two ranges of water contents: a low range from 4.0 × 10⁻³ to 5.0 × 10⁻² g g⁻¹ (6.6 × 10⁻³ to 8.2 × 10⁻² m³ m⁻³), and a partly overlapping ultralow range from 5.6 × 10⁻³ to 9.9 × 10⁻⁵ g g⁻¹ (9.9 × 10⁻⁵ to 1.6 × 10⁻² m³ m⁻³). These different water content ranges required two different types of diffusion cells (Figure 2) and different approaches for establishing initial salt concentrations as described below.

![Figure 2. Diffusion cells. a. Low water content diffusion cell. 1. Open diffusion cell with divider shim in place, and window facing down. 2. Moist “sink” side sand packed. 3. Moist “source” side sand packed. 4. Shim removed. 5. Compaction of sand to its final bulk density with PTFE back sheet, sealing with Kapton tape and back cover. 6. Assembled diffusion cell. 7. Photograph of diffusion cell with cover removed. b. Ultralow water content diffusion cell. 8. Exploded view of diffusion cell. 9. Assembled diffusion cell during filling with dry sand, and during diffusion with water films equilibrated with controlled humidity environment. 10. Diffusion cell with cover plate removed for X-ray microscope measurements. 11. Photographs of diffusion cell (unassembled, sand-filled).](image)

Low Water Content Systems. In these systems, separate solutions were prepared consisting of 1.5 M CsI for the sink half, and 50 mM RbBr with 1.5 M CsI for the source half. These solutions were added by pipet to their corresponding sink and source sands contained in individual scintillation vials, to achieve different water contents (4.0 × 10⁻³ to 5.0 × 10⁻² g⁻¹), quickly mixed with a spatula, and sealed with Al foil-line caps. The prewet samples were then stored for 2–8 days to allow more uniform distribution of water and solutes.

Each low water content diffusion cell consisted of a 6.35 mm thick acrylic sample frame to contain a 10 mm wide, 60 mm long diffusion region (30 mm long half-cells) with a 50 μm thick X-ray transparent polyimide (Kapton) window (Figure 2a). With the window and supporting cover sealed onto the bottom side of the frame, a stainless steel divider shim was secured at the midplane of the diffusion cell, and 2.35 g (equivalent dry mass of premoistened sand) of tracer-free sand was distributed within the cell on one side of the divider. The opposite side of the diffusion cell was filled with the same mass of tracer-containing sand (same water content). After leveling the sands on each side, the divider was removed, and a 10 × 60 × 0.16 mm thick PTFE (Teflon) sheet was pressed onto the sand and into the frame. Compression of the sands by the PTFE sheet facilitated contact between the two sand regions and established time zero for diffusion. With the upper surface of the PTFE sheet level with that of the acrylic frame, the sand was compressed to a bulk density of 1.64 g cm⁻³ (total porosity = 0.38). The PTFE backing was secured to the frame with Kapton tape and additional acrylic support plate, and stored in a high humidity (>99%) chamber at laboratory room temperature (23 ± 1 °C). Two days prior to X-ray microprobe measurements of diffusion profiles, these diffusion cells were doubly contained in humidified (moistened towels) plastic bags for shipment to the Advanced Photon Source at Argonne National Laboratory.

Ultralow Water Content Systems. For the driest sands, water contents were established by equilibration with fixed relative humidity (rh) environments which were controlled with saturated salt solutions. Although water vapor adsorption isotherms were determined on the sand for rh values ranging from 0.077 up to 0.97 (97%), diffusion profiles were only obtained on a subset of rh values ranging from 0.216 up to 0.923 because of disturbance of the contact plane in some of the cells described later. In order to minimize temperature variations in controlled humidity environments, adsorption isotherms and diffusion sample incubations were conducted in an incubator at 30.0 ± 0.5 °C. Sands for the source sides were prepared by first mixing in the inert TiO₂ as described previously, then wetting with a solution consisting of up to 200 mM KI and 5.0 mM RbBr (lower concentrations added to sands to be maintained at rh <0.22) to an initial water content of 6.0 × 10⁻² g g⁻¹. Sands for the sink sides of diffusion cells were prepared without TiO₂ and spiked only with KI (same ionic strength as applied to the source side, solution/sand = 6.0 × 10⁻² g g⁻¹). After spiking and thoroughly mixing solutions in each sink/source sand batch, sands were dried overnight at 60 °C, cooled to room temperature in a desiccator, and then each sample was further mixed prior to packing into a diffusion cell.

Each ultralow water content diffusion cell consisted of a 6.35 mm thick acrylic sample frame to contain a 10 mm wide, 40 mm long diffusion region (20 mm long half-cells), 50 μm thick X-ray transparent polyimide (Kapton) window, and a 160-mesh stainless steel screen backing to allow rapid adsorption of water vapor (Figure 2b). The assembled diffusion cell was vertically oriented, filled through the top channel with the dry “sink” sand up to the midplane (20 mm) in ~5 mm increments, and each increment lightly compacted to achieve a bulk density of 1.64 g cm⁻³. The remaining volume was similarly filled with the RbBr- and TiO₂-containing dry sand, and the access port was sealed.
Table 1. Water Vapor Adsorption Isotherms for Quartz Sand, 106-125 μm, at 30 °C, Comparing Sands without Salts, And with KI and RbBr Salts

<table>
<thead>
<tr>
<th>saturated salt solution for controlling rh</th>
<th>washed sand</th>
<th>sand with KI, RbBr salt</th>
</tr>
</thead>
<tbody>
<tr>
<td>relative humidity (30 °C)</td>
<td>water content, g g⁻¹</td>
<td>water film thickness, nm</td>
</tr>
<tr>
<td>LiBr</td>
<td>2.6 × 10⁻⁴</td>
<td>3.0 × 10⁻⁴</td>
</tr>
<tr>
<td>LiCl</td>
<td>3.7 × 10⁻⁴</td>
<td>4.4 × 10⁻⁴</td>
</tr>
<tr>
<td>K-acetate</td>
<td>5.4 × 10⁻⁴</td>
<td>5.6 × 10⁻⁴</td>
</tr>
<tr>
<td>MgCl₂•6H₂O</td>
<td>5.6 × 10⁻⁴</td>
<td>6.8 × 10⁻⁴</td>
</tr>
<tr>
<td>NaBr</td>
<td>6.4 × 10⁻⁴</td>
<td>7.6 × 10⁻⁴</td>
</tr>
<tr>
<td>NaCl</td>
<td>7.5 × 10⁻⁴</td>
<td>1.6 × 10⁻⁴</td>
</tr>
<tr>
<td>KCl</td>
<td>8.2 × 10⁻⁴</td>
<td>5.0 × 10⁻⁴</td>
</tr>
<tr>
<td>KNO₃</td>
<td>2.1 × 10⁻⁴</td>
<td>9.9 × 10⁻⁴</td>
</tr>
<tr>
<td>NaBr</td>
<td>3.3 × 10⁻⁴</td>
<td>1.43</td>
</tr>
</tbody>
</table>

*Conditions associated with diffusion measurements are indicated by asterisks.

2.4. Inverse Modeling to Determine $D_e$.

The 60 and 40 mm long diffusion cells were modeled as one-dimensional porous materials. The domain was discretized into 0.05 mm long elements, that is, at a resolution identical to the Rb concentration data. Rb transport is modeled as a Fickian diffusion process in the liquid phase only, that is, advective transport or multiphase diffusion effects are ignored. The model domain is divided in two halves, the left representing the Rb source zone, and the right the Rb sink zone. For modeling the low water content systems, the source and sink zones are separated by three grid blocks (i.e., a 0.15 mm wide zone) at the center of the diffusion cell. This zone represents the location of the removed divider, where the material may be disturbed and water films may have reduced contact compared to that in the undisturbed zones. Each of these three zones is allowed to have its own tortuosity factor used to calculate $D_e$.

Subdividing the experiment into three regions is motivated by the different treatments they underwent during sample preparation. While the thickness of the zone disturbed by the divider is unknown, an error in the assumed thickness will only affect the estimated diffusion coefficient of the disturbed zone, which is of no interest. Moreover, the assumption that the source and sink zones are essentially homogeneous appears justified by the fact that no distinct change in diffusion behavior is evident from the measured concentration profiles, and that no discrete changes in the residuals can be observed after calibration. Minimizing the number of regions (and thus number of parameters to be estimated) is desirable to avoid overparameterization of the inverse problem, which would lead to strong parameter correlations and consequently large estimation uncertainties. In these calculations, $n = 0.38$, $\theta$ and $S$ are set to their cell-specific values, and $D_o$ is set to $2.1 \times 10^{-9}$ and $2.4 \times 10^{-9}$ m² s⁻¹, at 23.0 and 30.0 °C, respectively.

Water contents in the source and sink halves of the cell are initialized as measured; they do not change during the simulation. Normalized Rb concentrations on the left and right are set to 1.0 and 0.0, respectively. The simulations were performed using the TOUGH2 simulator, with runs continued to the times corresponding to when the Rb profiles were measured with the X-ray microprobe. The main processes being simulated are multicomponent molecular diffusion under a local thermodynamic equilibrium assumption; advection was inhibited by specifying a permeability of zero. Each measured data point was included in the inversion. Measurement errors were assumed heteroscedastic, with $\sigma = 0.02c + 0.01$, where $c$ is the measured normalized Rb concentration (i.e., $c = C/C_o$), over times short enough that concentrations at external boundaries remain unchanged. The measured diffusion profiles revealed that uniform column packing was usually not achieved, motivating analyses through inverse modeling.
The weighted least-squares objective function was minimized using the Levenberg–Marquardt algorithm as implemented in iTOUGH2.57,58

3. RESULTS AND DISCUSSION

3.1. Adsorption Isotherms and Water Film Thicknesses. The saturated salt solutions, rh, gravimetric water contents, and water film thicknesses are shown in Table 1 for two substrates, clean washed sands and sands containing KI and RbBr at levels used to spike the source half of the ultralow water content systems. Although the surfaces of the sand have rough microtopography (Figure 3a), the low specific surface area (0.069 m² g⁻¹) indicates that intragranular uptake of water was insignificant. Thus, at low water contents, water resides largely as adsorbed films on grain surfaces and to lesser extent as pendular rings around grain–grain contact points. Adsorption isotherms similar to that obtained on the washed sands have been previously reported on flat Si-oxide and quartz surfaces,37,59 indicating that capillary condensation in the sand’s rough surfaces was minor. Water vapor adsorption isotherms for the salt-spiked sands exhibited two distinct regions delineated by the deliquescence relative humidity of the dominant salt, KI (rh 0.68 at 30.0 °C). Below this rh, water film thicknesses on the salt-treated sands were experimentally indistinguishable from values obtained in the washed (salt-free) sands. In contrast, hydration and dissolution of KI resulted in much greater water film thicknesses in the salt-treated sands (Figure 3b). The extent of film thickness increase was also

Figure 3. Quartz sands and water films associated with the ultralow water content diffusion experiments. a. Scanning electron micrographs of sands. b. Water vapor adsorption isotherms, comparing measurements on sands with isotherms from the literature obtained on flat silica surfaces. Influences of the KI and RbBr salts added to sands become significant above the deliquescence rh of KI.

Figure 4. Example diffusion profiles from the low water content (a–c) and ultralow water content systems (d–f).
influeced by the variable initial water/sand mass ratio achieved (4.0 × 10⁻³ to 5.0 × 10⁻² g g⁻¹) upon adding the KI solution. It should be noted that water vapor adsorption equilibrium times ranged from ∼0.2 days (rh < 0.33) to 2 days (rh = 0.923).

3.2. Measured Diffusion Profiles and Calculated $D_e$

Examples of normalized Rb diffusion profiles and matches obtained with the calibrated models are shown in Figure 4. The measured data are shown as blue symbols (individual points are averages of eight values obtained at a specific x position, with coefficients of variation typically ranging from 0.1 to 0.2), and the simulated concentration profiles are represented by solid red lines. Also shown in these graphs are normalized profiles for the inert Ti tracer used to locate the internal midplane boundary. It should be noted that collection of the Ti Kα profile was unsuccessful on one of the wettest systems (Figure 4a). However, Pb is a common impurity in anatase, and the Pb Lα (10.552 keV) profile exhibited a distinct step that allowed identification of the midplane location. The Ti and Pb profiles not only located the midplane position in each cell, but also helped determine if the integrity of each cell was suitable for obtaining diffusion measurements. Several of the cells did not exhibit sharp steps in Ti profiles, indicating mechanical disturbance of the sands. These cells were excluded from diffusion analyses.

The measured diffusion profiles were commonly asymmetric about the midplane (e.g., Figures 4b–d), indicative of differences in packing between the source and sink sections. Lower packing density at the interface region in some of the low water content systems is also evident from very steep Rb concentration gradients at the midplane (Figure 4b,c). Only a few of the cells exhibited symmetric diffusion profiles amenable to approximation as a homogeneous medium. The diffusion profile obtained by fitting eq 3 to the normalized Rb profile is indicated by the dashed green line in Figure 4a, where the fit $D_e$ of 2.59 × 10⁻¹¹ m² s⁻¹ (root-mean-square difference in concentration = 0.031) is between values obtained with TOUGH2 for the source and sink sides of the cell (2.84 × 10⁻¹¹ and 1.93 × 10⁻¹¹ m² s⁻¹, respectively).

The $D_e$ values obtained via inverse modeling of the diffusion profiles (and a few $D_e$ from fitting eq 3) are summarized in Figure 5a and b, with a logarithmic x axis used in the latter graph to facilitate examination of trends at very low θ. Included in this graph are literature $D_e$ values of other coarse-textured media that were expected to have negligible intragranular porosity, such that diffusion at low saturations would be
restricted to occur through adsorbed water films. Results of our measurements and calculations are in agreement with the general trend of decreasing \( D_v \) with decreasing \( \theta \), and to our knowledge extend the lower limits of measured solute diffusion in unsaturated media substantially lower than previous studies. Included in Figure 5a and b are lines representing \( \theta D_v \) for nominal room temperature (23 °C) and for 30 °C. Note that the \( D_v \) values generally reside within a moderately narrow, \( \theta \)-dependent band below the \( \theta D_v \) lines. Our experiments at the lowest \( \theta \) of 9.9 \( \times \) 10^{-5} and 1.1 \( \times \) 10^{-4} yielded \( D_v \) of 8.7 \( \times \) 10^{-15} and 1.1 \( \times \) 10^{-14} m^{2} s^{-1}, respectively.

The dominant influence of \( \theta \) on \( D_v \) becomes more apparent when considering the impedance factor \( f \), obtained by dividing the \( D_v \) values by their associated \( \theta D_v \). These \( D_v/(\theta D_v) \) are plotted with respect to \( \theta \) in Figure 5c. Note that over more than 3 orders of magnitude variation in \( \theta \), the \( f \) values vary only moderately, largely in the range between 0.02 and 0.5. These \( f \) values are replotted with respect to water film thickness in Figure 5d. For our quartz sands, measured \( \theta \) were divided by the product of bulk density (1.64 g cm^{-3}) times the specific surface area (0.069 m^{2} g^{-3}) to obtain values of average film thicknesses. For the other granular materials from the literature, their median diameters were selected, and specific surface areas were estimated as being 3.5 times that of spheres of these median diameters (3.5 being the ratio of BET-measured surface area denoted \( \Theta \)) divided by their associated \( \Theta \) or lines. Our experiments at the shaded region of Figure 5d exceed thicknesses strictly attributable to adsorption, and include significant contributions from capillarity at grain contacts, surface roughness, and potentially intragranular pores. We do not have an explanation for the rather wide variation in \( f \) measured over most of our tested \( \theta \), but note that similarly wide ranges in \( f(\theta) \) are typical of the data in the earlier literature as well (Figures 5c,d).

### 4. IMPLICATIONS FOR DIFFUSION IN THIN FILMS

Measurements of Rb⁺ and Br⁻ diffusion within adsorbed water films spanning 2 orders of magnitude in thickness (from about 100 nm down to 1 nm) were obtained through experiments in unsaturated, monodisperse, pure quartz sands. The limited reduction in the impedance factor \( f \) over a wide range in film thicknesses is consistent with some previous experimental and computational investigations that found only minor decreases in mobility of ions and water near solid surfaces. However, other studies involving clays and nanoscale fractures have reported more substantial decreases in water and ion mobility. Further tests are needed to determine the extent to which these contrasting conclusions reflect differences in confining environments; confinement between opposing solid–water interfaces of nanofractures and clay interlayers, versus adsorbed films bounded by solid–water and water–gas interfaces. In addition, experiments involving other cation–anion pairs having distinctly different hydrated radii and mineral surface interactions will be useful for better understanding mobility along interfaces. The approach developed here involving humidity control will be useful for further investigations of transport in adsorbed water films, particularly in the nm and subnm thickness range.

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**Notes**

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